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DESCRIPTION

FILM FOR FORMING VAPOR DEPOSITED BALLOON

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TECHNICAL FIELD

The present invention relates to a film for
5 forming a vapor deposited balloon and a method for
manufacturing the same.

BACKGROUND ART

Conventionally used as a film for forming a
vapor deposited balloon is a laminate film having a three-
10 layer structure consisting of a layer of nylon 6, an
adhesive resin layer and a layer of LLDPE.

Further, Japanese Unexamined Patent Publication
No. 290650/1995 proposes a laminate film having a five-
layer structure consisting of a polyamide resin layer, a
15 saponified copolymer layer of ethylene and vinyl acetate,
a polyamide resin layer, an adhesive resin layer and a
polyolefin resin layer.

These films, however, have the defect of curling.

An object of the present invention is to provide
20 a film for forming a vapor deposited balloon, which is
free of curling.

DISCLOSURE OF INVENTION

The present invention provides a film for
forming a vapor deposited balloon, the film having a five-
25 layer structure consisting of a polyamide resin layer, a

polyolefin layer, a polyamide resin layer, an adhesive resin layer and an LLDPE layer.

In the film for forming a vapor deposited balloon according to the invention, the polyamide resin layer comprises crystalline or amorphous nylon such as nylon 6 (poly- ϵ -caprolactam), nylon 66 (polyhexamethylene adipamide), nylon 12 (a polymer of lactam of 12-aminododecanoic acid), nylon 6-66 copolymer, nylon 6-12 copolymer or the like. The polyamide resin layer preferably comprises about 70-95 wt.% of crystalline nylon and about 30-5 wt.% of amorphous nylon, more preferably about 80-90 wt.% of crystalline nylon and about 20-10 wt.% of amorphous nylon. Nylon 6-66 copolymer is a copolymer of nylon 6 (poly- ϵ -caprolactam) and nylon 66 (polyhexamethylene adipamide), and preferably contains nylon 6 in a proportion of about 30 mole % or more, more preferably about 50 mole % or more, further more preferably about 70 mole % or more. The nylon copolymer preferably has a molecular weight of about 13,000 to about 33,000. The two polyamide resin layers of the film may be the same or different as long as they contain the above components. Each polyamide resin layer has a thickness of about 1-15 μm , preferably about 3-10 μm . Examples of amorphous nylons include copolymers or terpolymers of dicarboxylic acid (e.g., terephthalic acid and isophthalic

acid) and diamine (e.g., hexamethylenediamine).

Any polyolefin layer that is capable of bonding the two polyamide resin layers together can be used without limitation. The polyolefin layer preferably comprises polyolefin such as polyethylene or polypropylene, more preferably linear low density polyethylene (LLDPE) and/or low density polyethylene (LDPE), especially LLDPE. The polyolefin layer has a thickness of about 1-6 μm , preferably about 1.5-4 μm . The polyolefin layer may contain, in addition to or in place of polyolefin such as LLDPE, a polyolefin-based adhesive resin such as grafted LLDPE. The polyolefin layer preferably comprises a polyolefin-based adhesive resin.

Any adhesive resin layer that is capable of bonding the polyamide resin layer and the seal layer together may be used without limitation. A preferred adhesive resin is LLDPE treated by graft reaction. The adhesive resin layer has a thickness of about 1-6 μm , preferably about 1.5-3 μm .

The seal layer comprises LLDPE or LDPE, especially LLDPE. The seal layer has a thickness of about 2-20 μm , preferably about 5-10 μm .

The total thickness of the layers of the film for forming a balloon according to the invention is about 10-70 μm , preferably about 15-35 μm .

Preferably, the polyamide shrinkable multilayer film of the invention is a flat film. The layers of the film are co-extruded from a T-die into a flat film and the film is subjected to simultaneous or sequential biaxial stretching. The laminate film may be formed by any method without limitation, but generally formed by extrusion casting on a chilled roll. The film thus obtained is simultaneously or sequentially stretched in biaxial directions, thereby giving a film of the invention. The stretching may be carried out in the machine direction using a roll stretching machine and in the transverse direction using a tenter stretching machine.

The stretch ratio in machine direction is about 1.2-5 and the stretch ratio in transverse direction is about 2.5-5. Stretching in machine direction is carried out at about 60-120°C, preferably about 70-100°C. Stretching in transverse direction is carried out at about 70-180°C, preferably about 100-160°C.

After stretching, heat treatment may optionally be carried out. There is no limitation on the heat treatment method, but the heat treatment is generally carried out by a continuous process after transverse stretching using a tenter stretching machine. The heat treatment may be carried out with the film being diminished (relaxed) in width by 20% or less, preferably

by 3-10%, or with the film being set to the same width as when transversely stretched or set to a larger width than when transversely stretched. The heat treatment may be carried out at temperatures below 150°C, preferably at about 80-130°C, optionally with the film being diminished in width by 20% or less, preferably by 3-10%, for example, using a tenter stretching machine. The film is subjected to thermal contraction in order to prevent natural contraction.

10 The multilayer film of the present invention is suitable for use as a film for forming a vapor deposited balloon. Stated more specifically, a vapor deposited layer of aluminium oxide, silicon dioxide or any other metal (e.g., aluminum foil) may be formed over the whole or partial surface of the outermost polyamide resin layer of the film of the invention. The metal deposited layer may be formed on any part of the surface of the outermost layer. However, it is preferable that the film be cut into strips and a metal vapor deposited layer be formed on one side of the centerline in width, with the other side being a transparent film. This is convenient because with use of such a film, one can very easily form a balloon having a transparent half side and a non-transparent metal deposited layer formed on the other half side. Moreover, 25 by using the film, one can easily form a spherical balloon

having a transparent appearance in one hemisphere and a non-transparent metal deposited layer formed on the other hemisphere.

- Preferably, the balloon film of the present invention has the following physical properties:
- Haze (measured according to ASTM D-1003): 1.0-7.0%, preferably 2.0-5.0%;
 - Tensile strength: MD (800-1500 kg/cm²), TD (800-1500 kg/cm²);
 - 10 • Tensile elongation: MD (80-180%), TD (80-180%);
(tensile strength and tensile elongation both measured according to JIS K-6732);
 - Thermal shrinkage (measured in warm water at 100°C for 30 seconds): MD (0-5.0%), TD (0-5.0%);
 - 15 • Puncture strength: NY surface (0.5 kg or more);
LL surface (0.5 kg or more) (measured according to JIS P-8116);
 - Impact strength: NY surface (5.0 kg·cm or more);
LL surface (5.0 kg·cm or more) (measured with
20 a punching impact tester using a small ball);
 - Seal strength (pressure = 2kg/cm²; time = 1 second):
120°C (1.0 kg/cm or more), 130°C (1.0 kg/cm or more),
140°C (1.5 kg/cm or more), 150°C (1.5 kg/cm or more),
160°C (1.5 kg/cm or more), 170°C (1.5 kg/cm or more);
 - 25 • Oxygen permeability: 100 cc/m²·24h·20°C×65%RH or less

(measured according to ASTM D-3985);

- Wet tension strength: NY surface (45 dyn/cm or more)
(measured according to JIS K-6768);

- Slipperiness: between NY-NY surfaces (both the
5 coefficient of static friction and the coefficient of
dynamic friction being 0.3 to 0.6);
between LL-LL surfaces (both the coefficient of static
friction and the coefficient of dynamic friction being
0.3 to 0.8) (measured according to ASTM D-1894).

10 The balloon of the present invention can be
formed by heat sealing portions of seal layer(s) of the
balloon film(s) together to form into a desired shape such
as sphere, ellipse or the like in a desired size.

BEST MODE FOR CARRYING OUT THE INVENTION

15 The present invention will be described below in
more detail with reference to Examples and Comparative
Examples.

[Curling Evaluation Method]

Measurement temperature and humidity: 20°C and
20 50%RH

(1) a film, 100 mm x 100 mm, is diagonally cut to make
incisions,

(2) the width and height of the film are measured after
rolling up the film in the machine direction and in the
25 transverse direction.

Criteria:

The larger the width is, the smaller curling property the film has (the quality is good).

The greater the height is, the smaller curling property the film has (the quality is good).

This is because a film having higher curling property is rolled up tightly, thus having a smaller width and a lower height.

Example 1

The laminate film having a five-layer structure was formed using the following starting materials.

(1) Starting materials:

- Polyamide resin layer (hereinafter referred to as layer "A") = nylon 6 (80 wt.%) and amorphous nylon (20 wt.%).
- Polyolefin layer (hereinafter referred to as layer "B") = an LLDPE based adhesive resin
- Adhesive resin layer (hereinafter referred to as layer "C") = an LLDPE based adhesive resin
- Seal layer (hereinafter referred to as layer "D") = LLDPE

(2) Production method

The layer components (A/B/A/C/D) were coextruded from a T-die to form a flat five-layer film on a chilled roll with cooling water being circulated. The film was then stretched three times in the machine direction using

a roll stretching machine at 80°C and stretched 3.8 times in the transverse direction using a tenter stretching machine in an atmosphere at 120°C. Subsequently, with the width of the film being reduced by about 4% using the
5 tenter stretching machine, the film was thermally fixed in an atmosphere at 200°C. The film obtained had a thickness of A/B/A/C/D = 4/2/4/2/8 (μm).

Table 1 shows physical properties of the film.

Example 2

10 A laminate film having a five-layer structure consisting of A/B/A/C/D = 4/2/4/2/8 (μm) in thickness was formed in the same manner as in Example 1 except that the following starting materials were used. Table 1 shows physical properties of the film.

15 Layer A = nylon 6 (80 wt.%) and amorphous nylon (20 wt.%)
Layer B = LLDPE based adhesive resin (50 wt.%) + LLDPE (50 wt.%)
Layer C = LLDPE based adhesive resin
Layer D = LLDPE

20 Example 3

A laminate film having a five-layer structure consisting of A/B/A/C/D = 6/3/6/2/18 (μm) in thickness was formed in the same manner as in Example 1 except that the following starting materials were used. Table 1 shows
25 physical properties of the film.

Layer A = nylon 6 (80 wt.%) and amorphous nylon (20 wt.%)

Layer B = LLDPE based adhesive resin

Layer C = LLDPE based adhesive resin

Layer D = LLDPE

5 Physical properties of the films obtained in
Examples 1-3 were determined according to the following
methods:

- Haze: measured according to ASTM D-1003;
- Tensile strength and tensile elongation: measured
10 according to JIS K-6732;
- Slipperiness (static friction/dynamic friction):
 measured according to ASTM D-1894;
- Thermal shrinkage: measured in warm water at 100°C for
 30 seconds;
- 15 • Puncture strength: measured according to JIS P-8116;
- Impact strength: measured with a punching impact tester
 using a small ball;
- Seal strength: measured at a pressure of 2kg/cm² for 1
 second;
- 20 • Oxygen permeability: measured according to ASTM D-3985;
- Wet tension strength: measured according to JIS K-
 6768;

Table 1

		Example 1	Example 2	Example 3
	Average thickness (μm):	20.7	20.5	35.0
	Haze (%):	2.5	3.2	6.5
5	Tensile strength (kg/cm^2)			
	MD	960	854	819
	TD	1397	1260	1140
	Tensile elongation (%)			
	MD	160	154	150
10	TD	85	95	92
	Slipperiness (static friction/dynamic friction)			
	NY-NY	0.58/0.51	0.49/0.42	0.46/0.38
	LL-LL	0.62/0.51	0.50/0.42	0.40/0.36
	Thermal shrinkage (%)			
15	MD	2.3	1.8	1.4
	TD	1.3	0.8	0.5
	Puncture strength (kg)			
	NY surface	0.67	0.72	0.95
	LL surface	0.60	0.62	0.75
20	Impact strength ($\text{kg}\cdot\text{cm}$)			
	NY surface	8.3	9.0	9.8
	LL surface	9.0	9.5	10.8

Table 1 (continued)

		Example 1	Example 2	Example 3
	Seal strength (kg/cm)			
	1 2 0°C	1. 2	1. 2	1. 9
5	1 3 0°C	2. 1	2. 3	3. 4
	1 4 0°C	2. 2	2. 2	3. 5
	1 5 0°C	2. 3	2. 3	3. 6
	1 6 0°C	2. 3	2. 3	3. 7
	1 7 0°C	2. 3	2. 2	3. 7
10	Oxygen permeability			
	(cc/m ² ·24h·20°CX65%RH)	4 3	4 2	4 0
	Wet tension strength (dyn/cm)			
	L L surface	3 6	3 6	3 6
	N Y surface	5 0	5 0	5 0

15 Comparative Example 1

A laminate film having a three-layer structure consisting of A/C/D = 10/2/10 (μm) in thickness was formed in the same manner as in Example 1 except that the following starting materials were used. The curing of the film obtained was measured. Table 2 shows the results.

Layer A = nylon 6 (80 wt.%) and amorphous nylon (20 wt.%)

Layer C = LLDPE based adhesive resin

Layer D = LLDPE

Test Example 1

25 The films obtained in Example 1 and Comparative

Example 1 were tested for curling. Table 2 shows the results.

Table 2

5	<u>Width (mm)</u>		<u>Length (mm)</u>	
	MD	TD	MD	TD
	Example 1	8-10	7-9	10-12 15-17
	Comp. Ex.1	5	5	5 5

Example 4

10 The film obtained in Example 1 was cut into strips having a width of 100 cm. A metal vapor deposited layer of aluminum was formed to a thickness of 400Å on one half of the surface of layer (A), i.e., on one side of the centerline in width. The obtained strips of the balloon film were formed into a spherical shape by heat
15 sealing portions of seal layers of the strips together. By feeding therein helium gas at 1.2 atm., a balloon having a non-transparent metal deposited layer was formed. The balloon thus obtained had a good design effect and floated in the air for 7 days.